
h(t) reconstruction and validation

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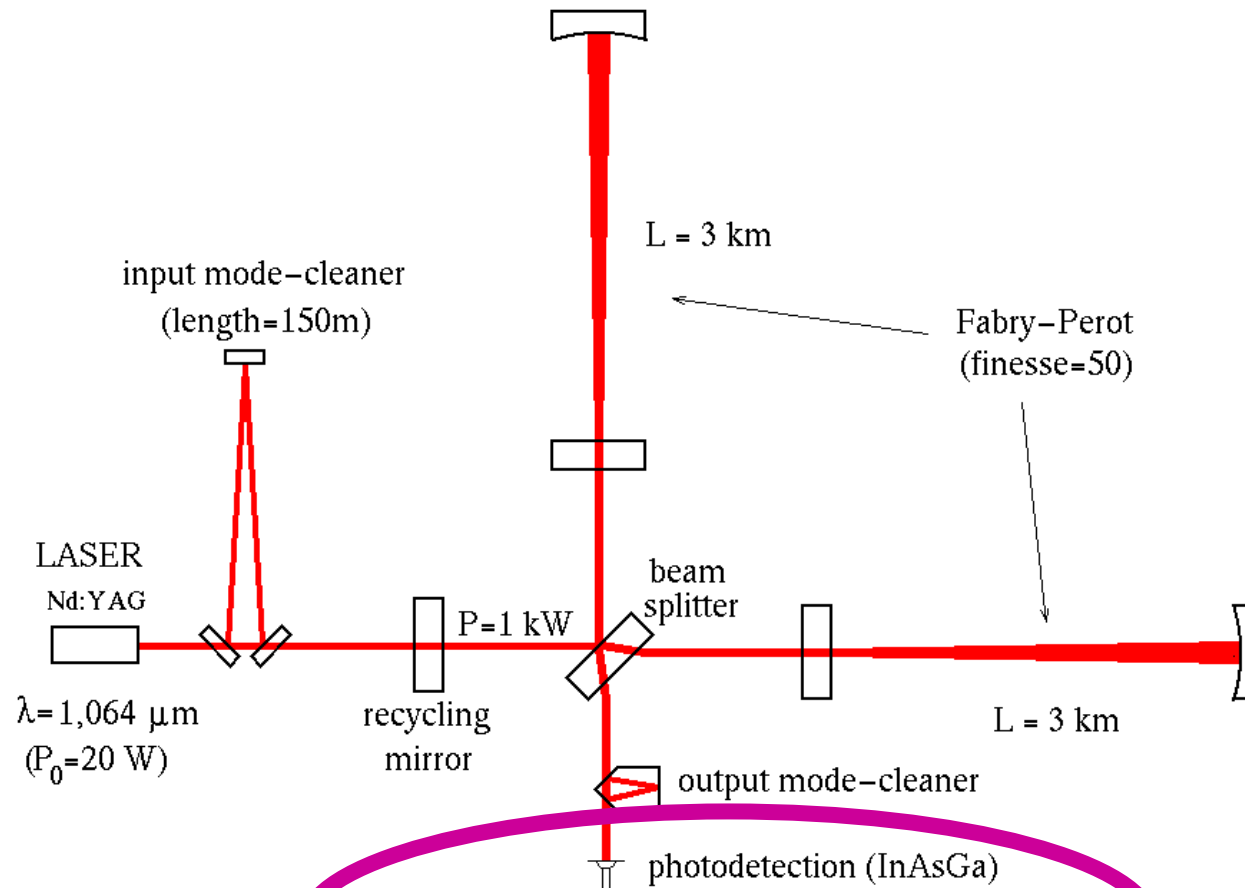
Gravitational Wave Data Analysis Workshop
IHP Paris

Outline

- Why do we need an $h(t)$ reconstruction?
 - ◆ The controls
 - ◆ The time domain approach vs frequency domain
- Measuring the basic calibration factors
 - ◆ The actuators gain
 - ◆ The transfer function
- Building $h(t)$
 - ◆ Frequency dependence effect
 - ◆ Noise subtraction
- Validation
 - ◆ Comparing the sensitivity curves
 - ◆ The shot noise level
 - ◆ The photon calibrator
 - ◆ Hardware injection

Remark: use Virgo examples; work in progress: not final results

Virgo Optical Configuration



First calibration task:

Volts \rightarrow meters?

The control challenge

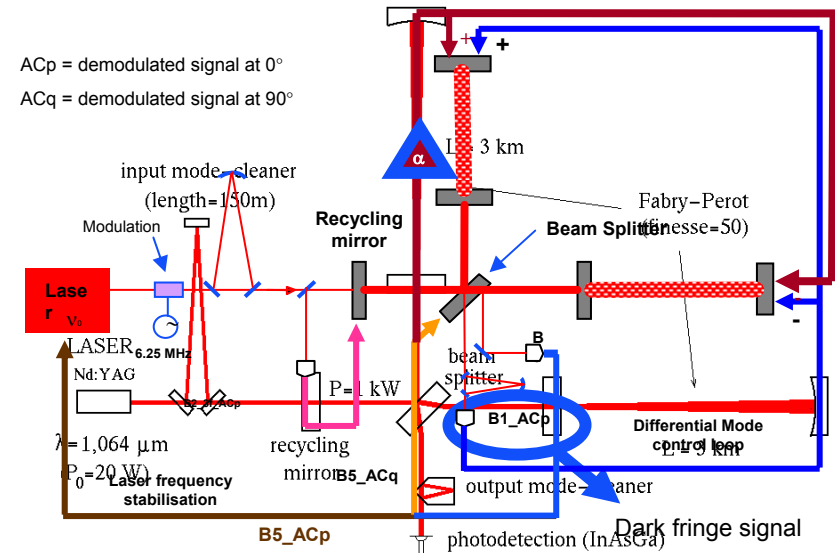
- Mirrors must be free test masses

- ◆ The free mirror motions is of several μ

- The ITF needs

- ◆ The mirrors at the right place

- » BS on the dark fringe
- » Locked F.P. and recycling cavities



- Contradiction solved by the Locking strategy

- ◆ Control the mirror at low frequency
- ◆ Mirrors are free at high frequency

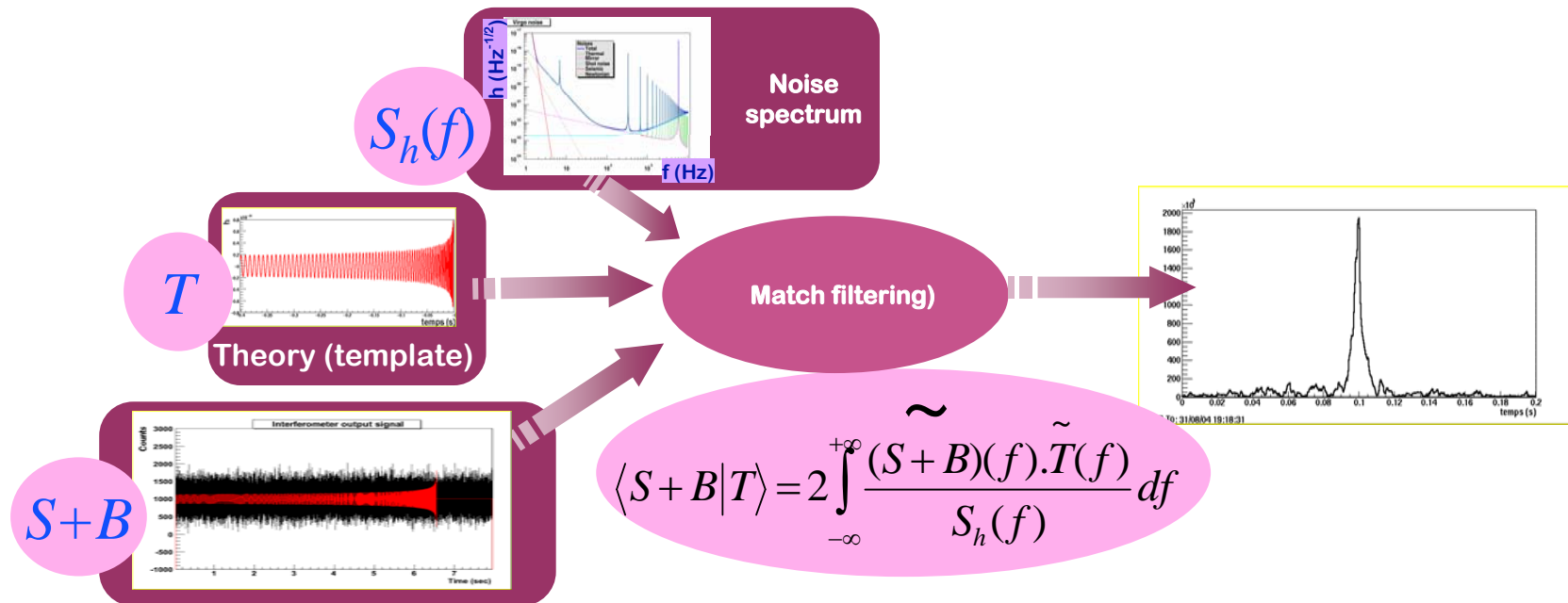
→ Distortion of the dark fringe signal

→ Transfer Function (TF): **Shape and Scale**

Second Calibration task: correct the control effects

Handling the TF: Frequency domain approach

- A lot of analysis works in the frequency domain
 - ◆ Example: Match Filtering for Binaries



- Some others analysis use a narrow or high frequency band:
 - ◆ require a simple procedure
- Need to get the right TF: time dependant
 - ◆ Data base required...

Handling the TF: time domain approach

- Correct the error signal and produce a time series: $h(t)$
- No more need of a data base from the user
 - ◆ Use only one channel: $h(t)$
- Will allow a additional bonus:
 - ◆ Some noise subtraction is possible

- But before: needs to get all inputs for the corrections

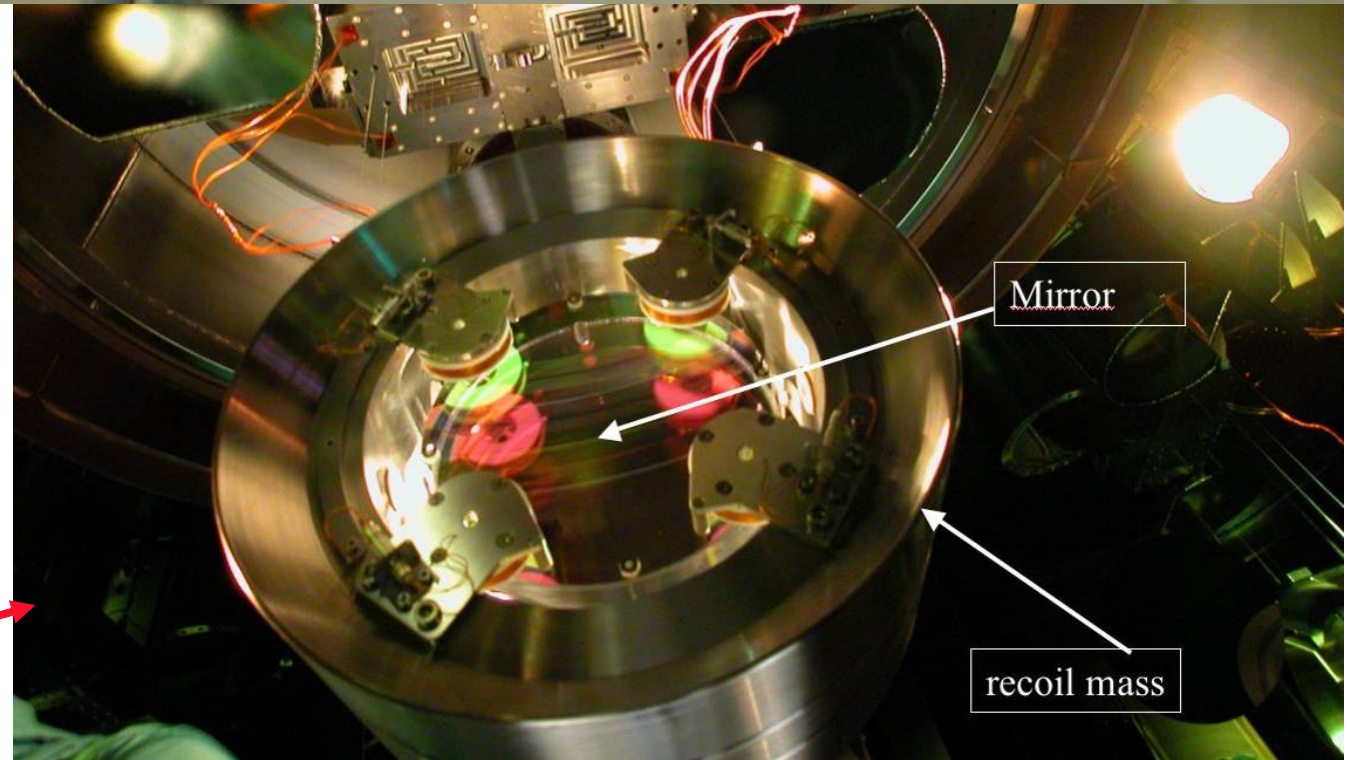
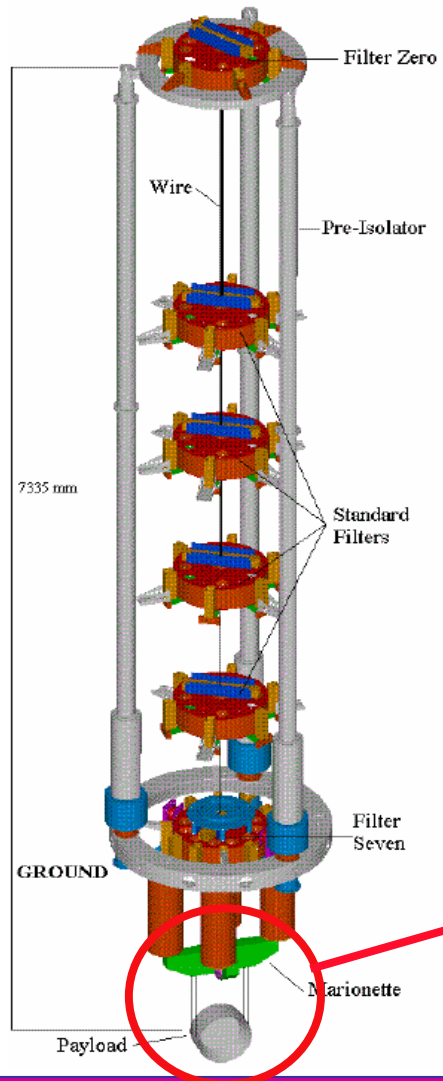
Extracting the calibration parameters

1) The scale

Need to push to mirror in a known way:

Actuator gain: $1V \rightarrow X$ meters?

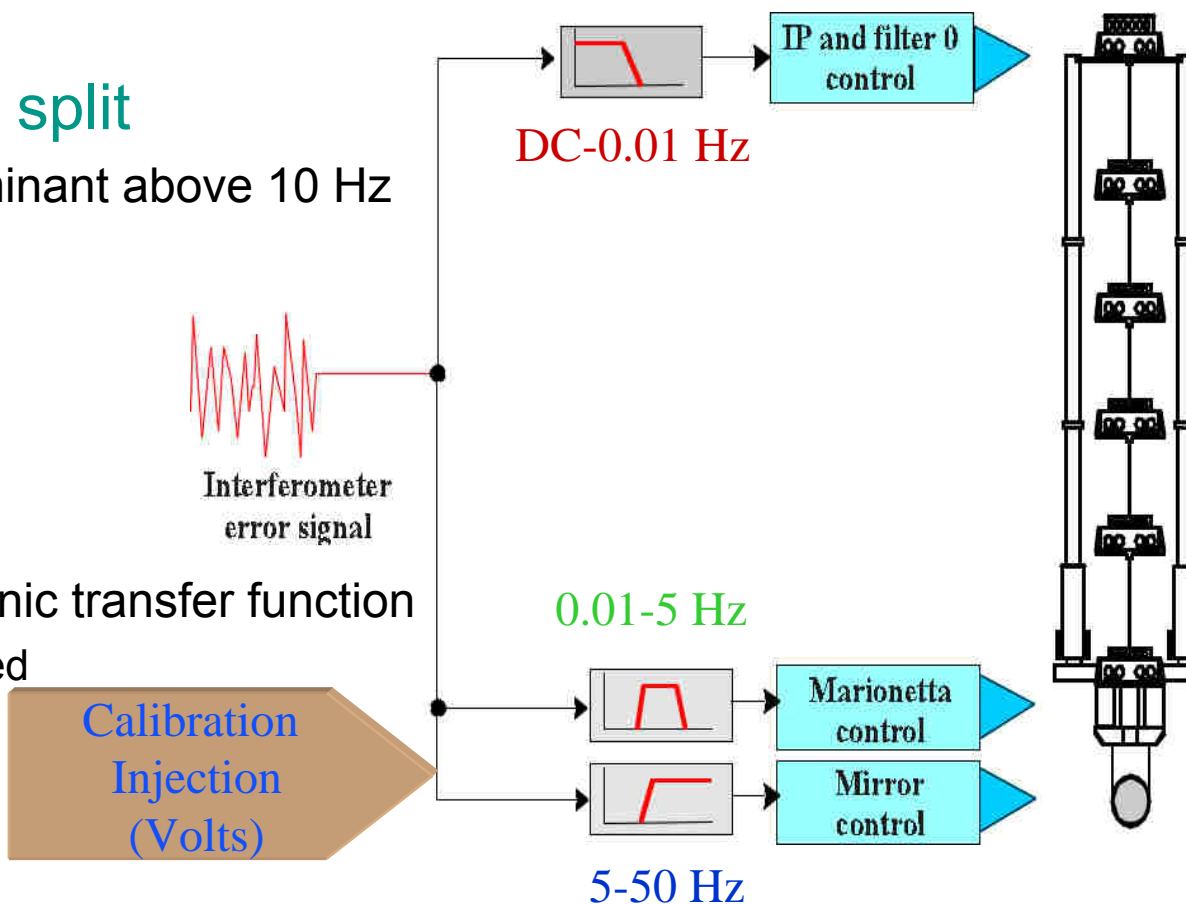
Mirror actuators



Virgo mirror controls

- Control signals are split
 - ◆ Reference mass dominant above 10 Hz

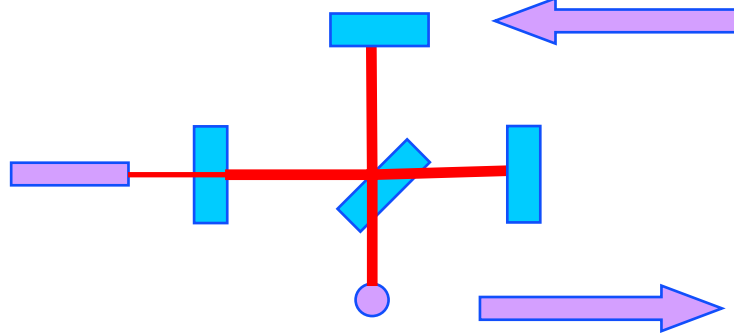
- Last stage model:
 - ◆ Simple pendulum
 - ◆ Assume a flat electronic transfer function
 - » More checks needed



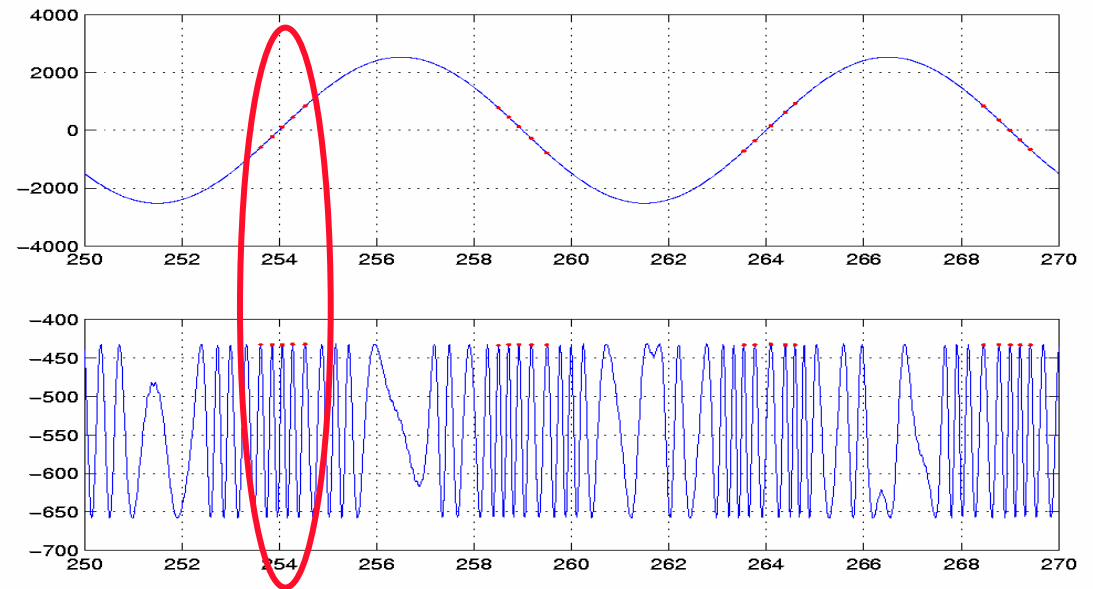
Actuator gain measurement: fringe counting

- Simple Michelson:

- ◆ Push the mirror over several fringes
- ◆ Extract gain from the DC power



- ◆ $P = P_0/2(1+C.\cos(2\pi\Delta L/\lambda))$



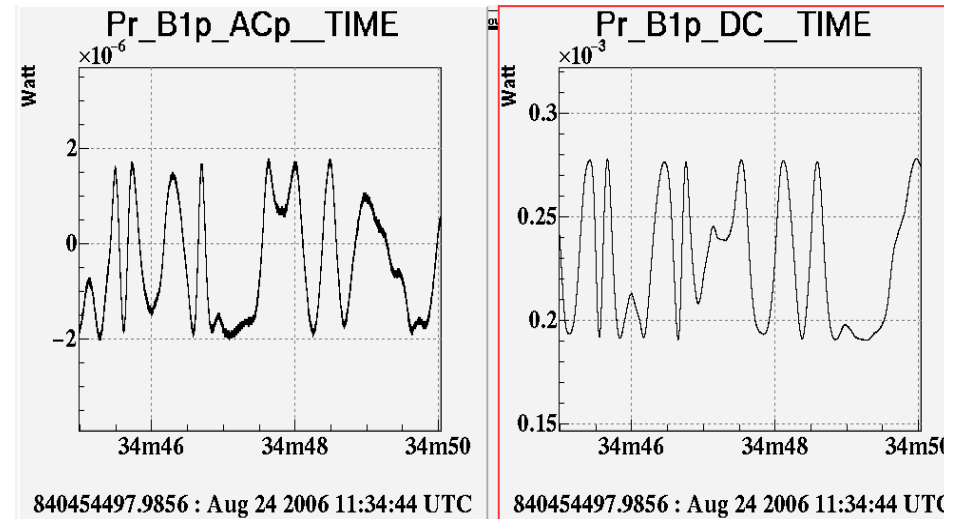
Time (s)

- Remark:

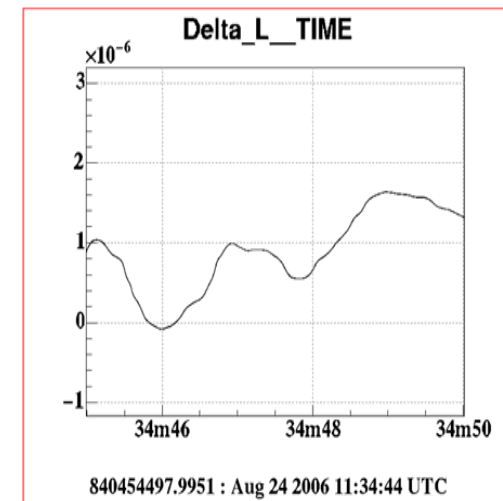
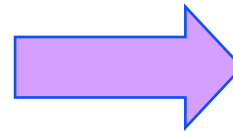
- ◆ need large displacement and a quite site
- ◆ Measure at low frequency

Open loop Michelson Reconstruction

- Monitor the DC and AC signals
 - ◆ AC signal is shifted by 90° from DC
 - ◆ Get the Power and the ITF contrast
 - » $P_{DC} = P_{0DC}/2(1+C.\cos(2\pi\Delta L/\lambda))$



- Invert the Michelson equation
 - ◆ non linear process
 - ◆ Get $\Delta L(t)$



- Absolute scale given by laser wavelength

Using the Open loop Michelson

- ITF Configurations

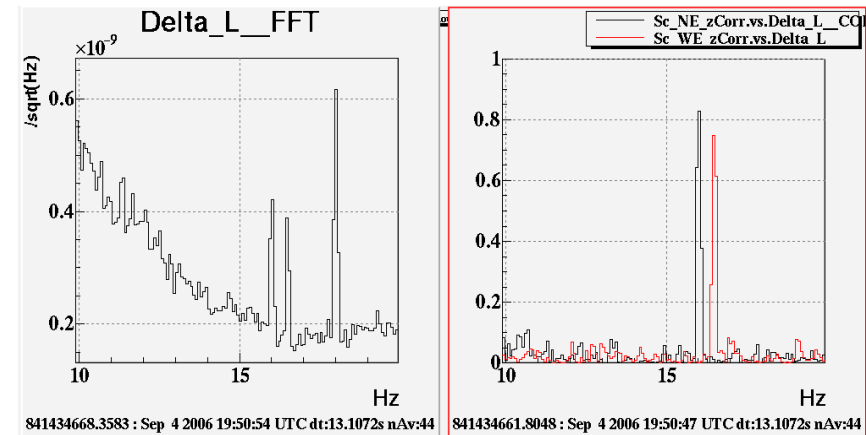
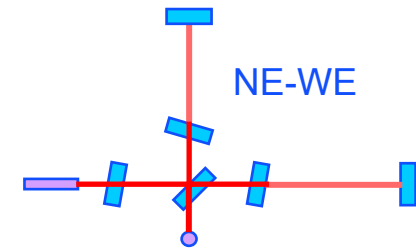
- ◆ Asymmetric (NE-WI;NI-WE) or long (NE-WE) Michelson

- Measurements:

- ◆ Inject “calibration lines”
- ◆ Take the transfer function (dL/zCorr)
- ◆ Rescaled by $(\text{frequency}/.6)^2$

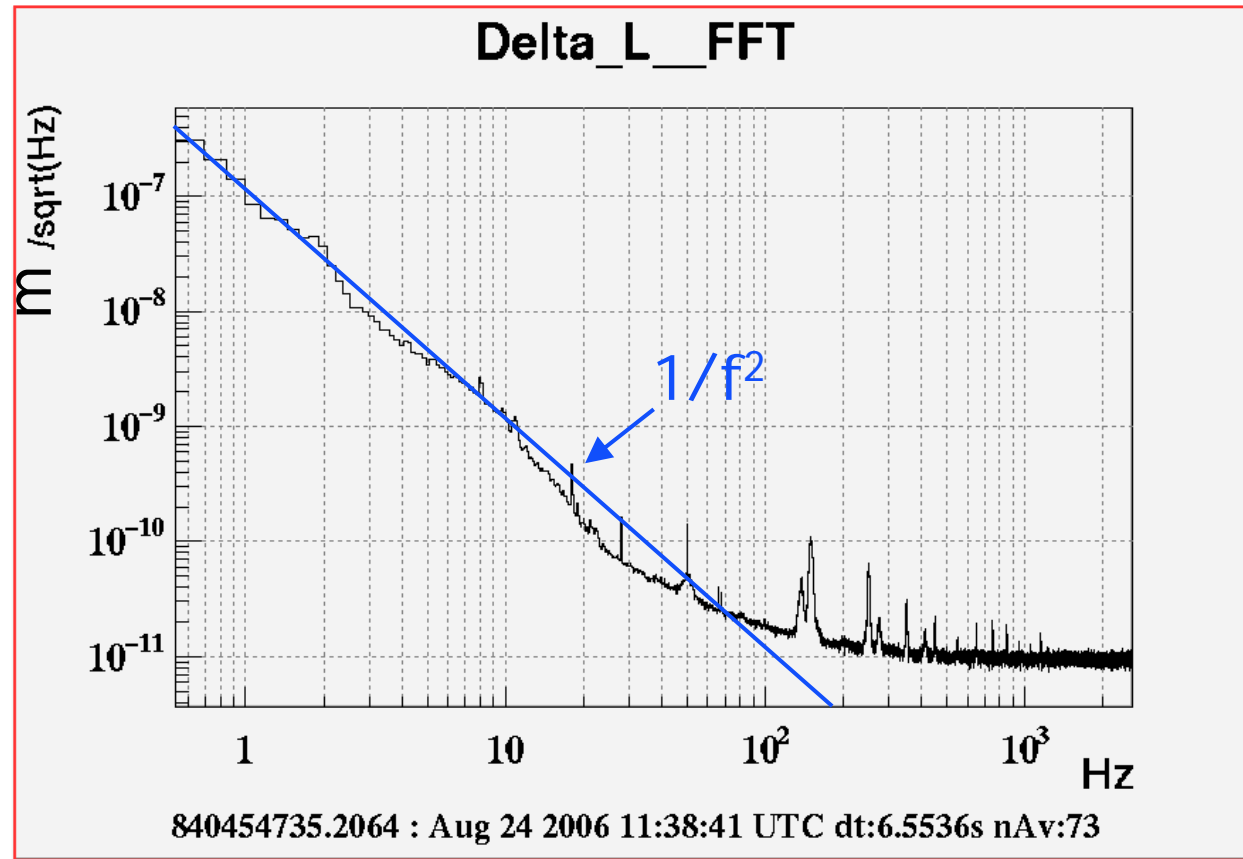
- Typical Results (Sep 4):

f [Hz]	ITF	Ampl.*601 [V]	WE Gain μV
26.5	Asym	3	11.6 ± 1.1
26.5	Asym	4	12.3 ± 1.7
26.5	Asym	6	11.9 ± 1.3
26.5	Long	6	12.8 ± 1.1
26.5	Asym	8	11.7 ± 0.9
16.5	Asym	6	12.2 ± 0.4
16.5	Long	6	12.5 ± 1.0
116.5	Asym	6	7.9 ± 3.6
Mean	Value	-	12.14 ± 0.30



Only statistical errors

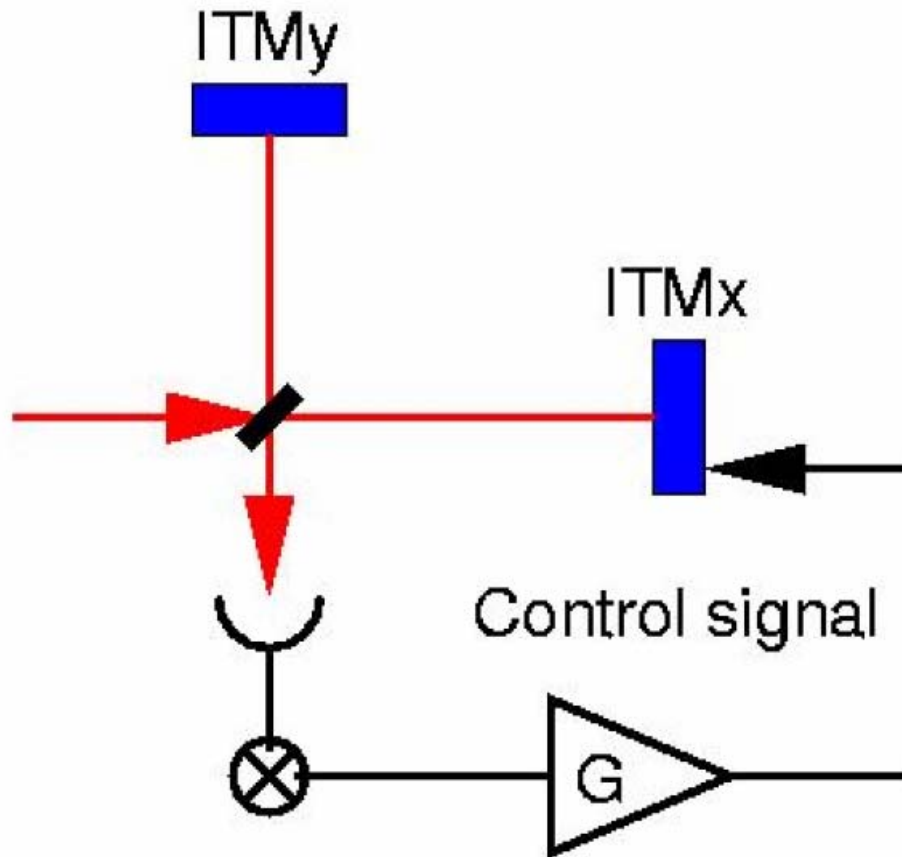
Typical Noise spectrum (WI-NE)



- Best sensitivity around 20-30Hz
 - ◆ No measurement above ~ 100 Hz

Another method: ITM fringe toggling

*Used by LIGO
(slide from M. Landry)*



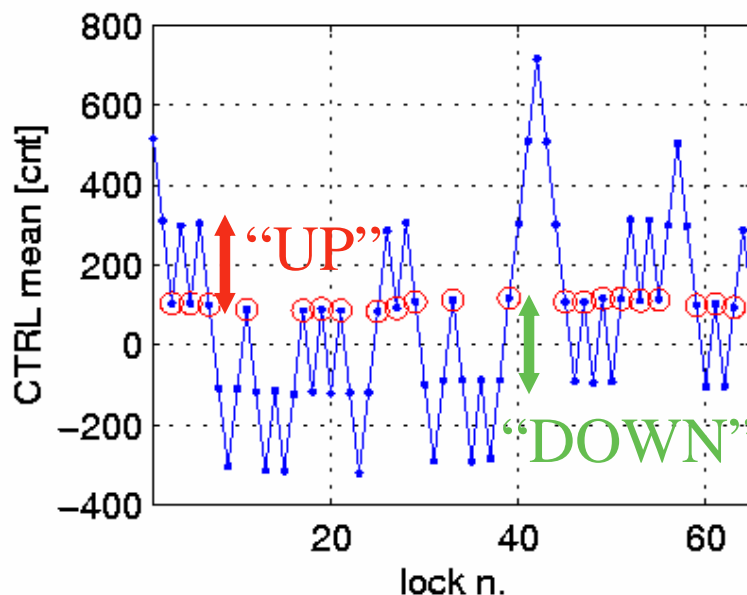
1. Lock Michelson on dark/bright fringe
2. Wait N seconds
3. $G \rightarrow -G$, Michelson transitions to bright/dark fringe
4. Goto step 2

$\lambda/4$ transition

Calibration of control signal

Fringe toggling analysis

Mean of MICH control signal for a given time stretch



*Used by LIGO
(slide from M. Landry)*

Mean (cnt) = 201.6607 +- 5.9289

---> (1.319e-09 +- 3.878e-11) [m/cnt]

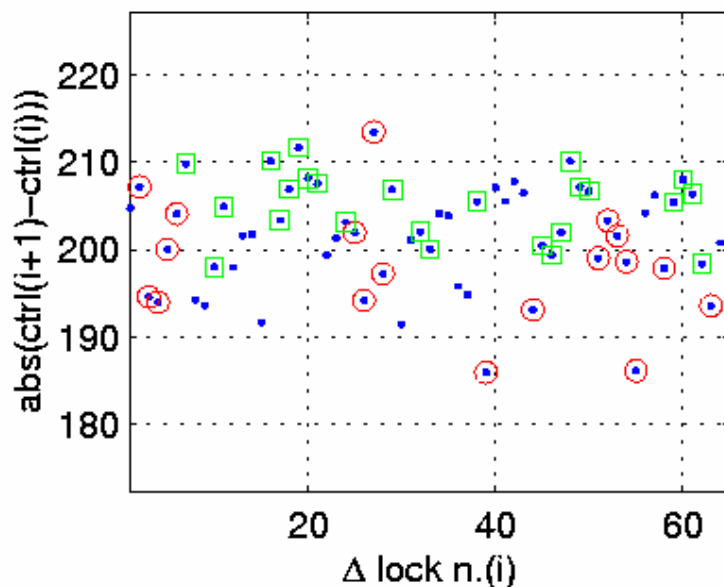
Mean UP(cnt) = 198.1013 +- 6.8505

Mean DOWN(cnt) = 205.0896 +- 3.9418

Mean SUM(cnt) = 403.1908 +- 7.9036

---> (1.3195e-09 +- 2.5865e-11) [m/cnt]

Difference of control signal between two successive locked stretches



H1:LSC-ITMY
1.32x10⁻⁹ m/count,

Sigma:
0.03x10⁻⁹

Actuators gain: some challenges

- The actuators gains are measured:
 - ◆ At low frequencies (“DC”)
 - » But used in a wider frequencies band
 - ◆ With large amplitude
 - » But used with lower signal (problem of the injected noise)
 - » Coil drivers have variable gain or frequency dependant responses (“whitening”)
- Need to cross check the electronic
 - ◆ Measure to know the coil driver Transfer Function
- Need to pay attention to the mirror mechanical model
 - ◆ near the pendulum resonance (0.6Hz for Virgo)
 - ◆ mirror internal mode (kHz band)
- Not all mirror actuators directly measured
 - ◆ Some optical configuration makes the life more complicate
 - » signal recycling, high finesse
 - ◆ Need to transfer measurements from one mirror to another mirror
 - » Use for instance locked cavities with closed calibration lines on all mirrors

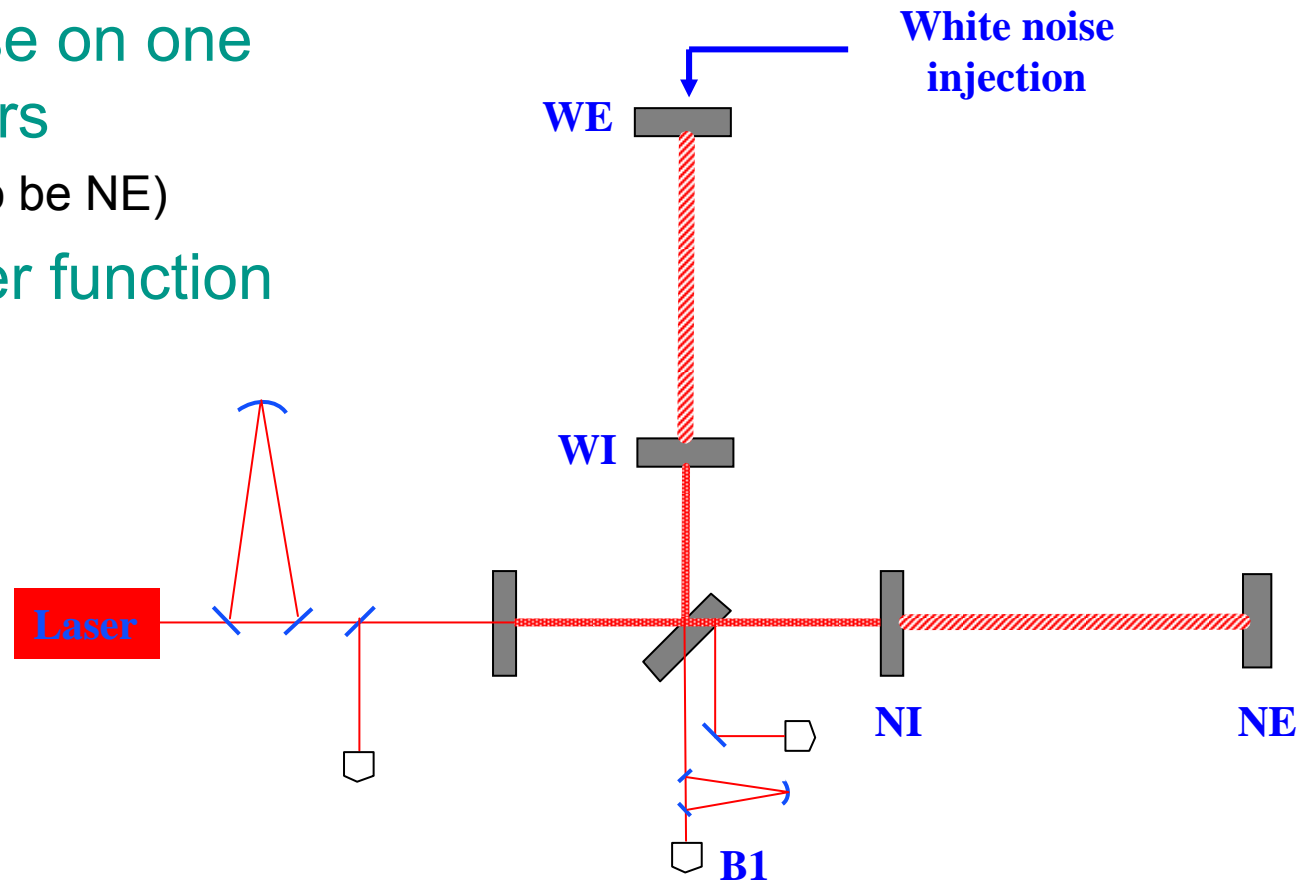
Extracting the calibration parameters

2)The shape

Measuring the Transfer function

TF Measurement

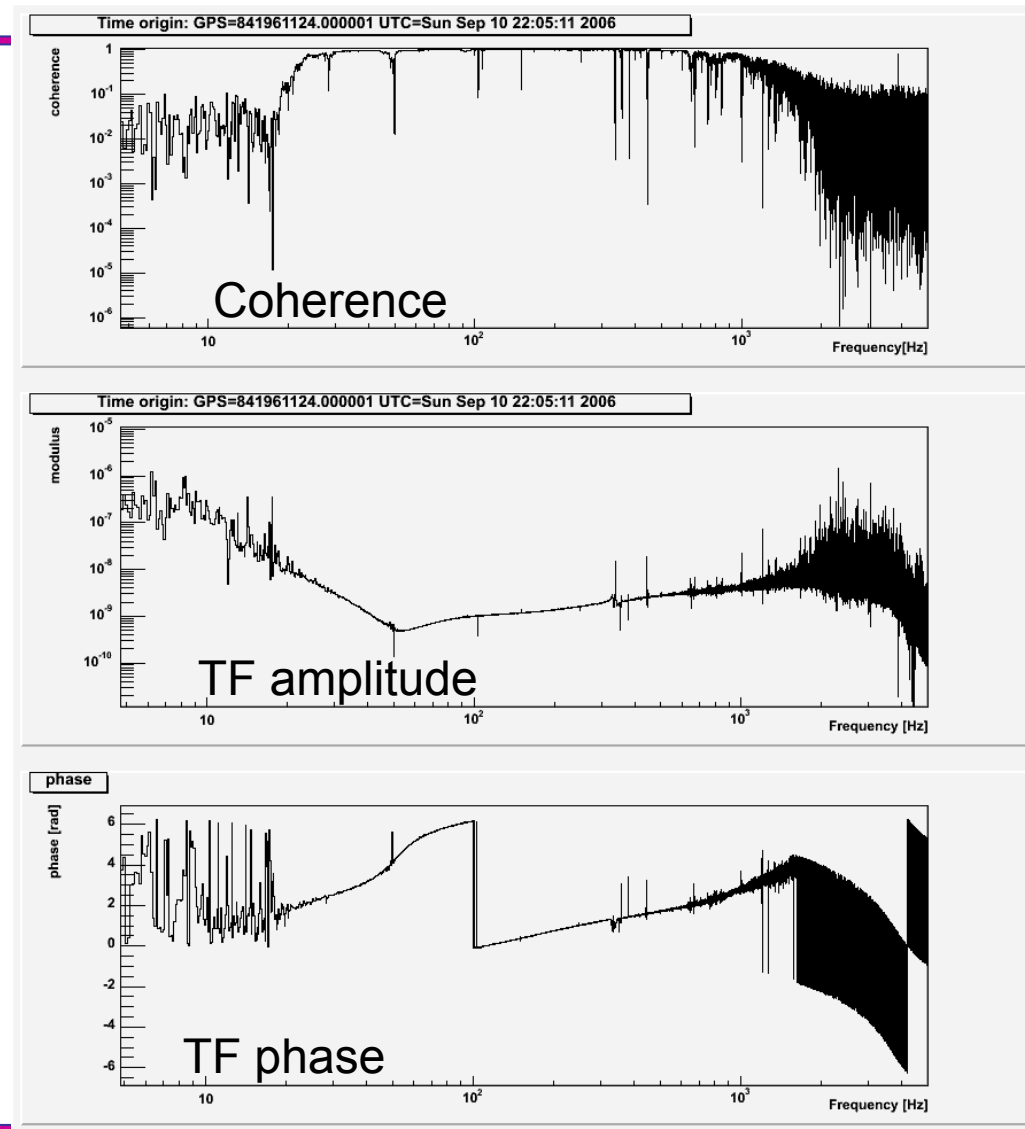
- Inject white noise on one of the end mirrors
 - ◆ Now WE (used to be NE)
- Measure transfer function to B1_ACp



Example of measured TF

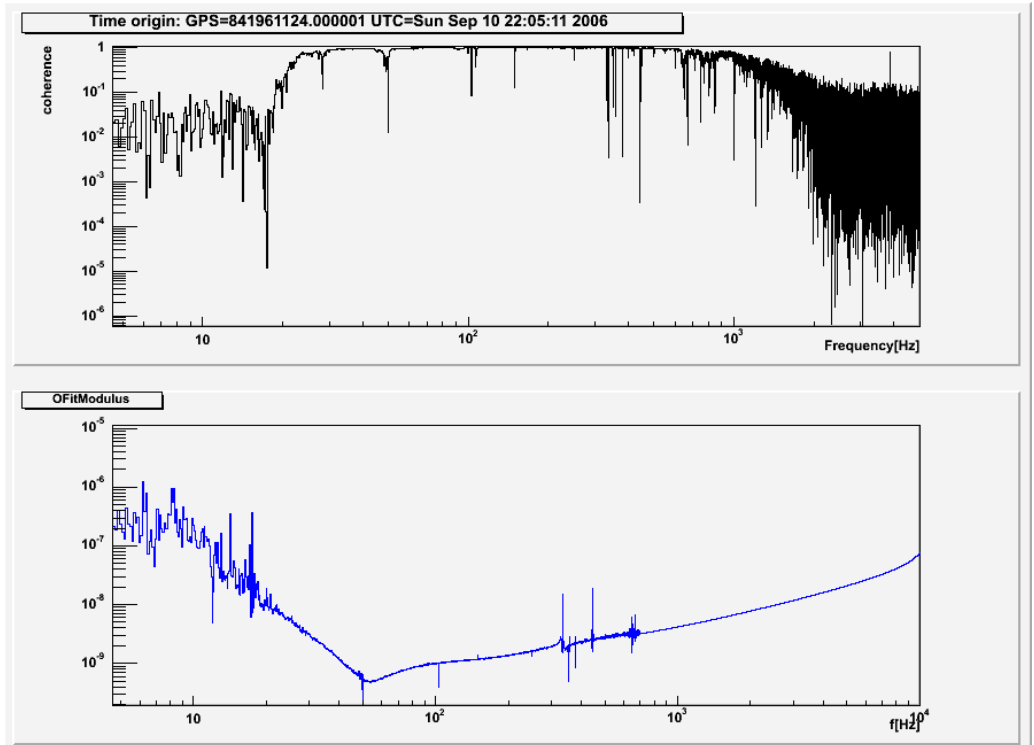
- White noise applied on mirror

⇒ Coherence typically between 30 and 700 Hz



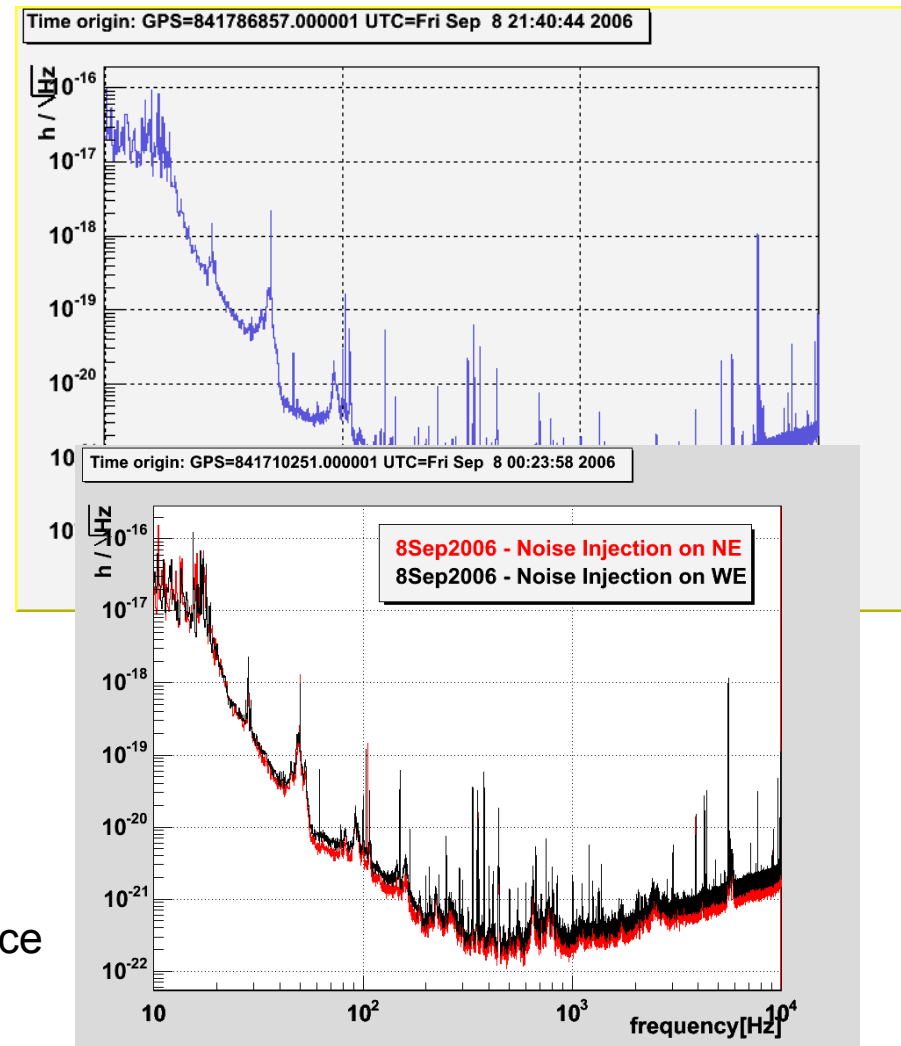
Model used

- Use raw transfer function in frequency band with good coherence (<700 Hz)
- Use fit above 700 Hz
 - ◆ Optical response with 2 free parameters: gain & delay
 - ◆ Cavity pole kept fixed @ 500 Hz
 - » Finesse of cavities well known
 - $F_{\text{North}} = 49.0 \pm 0.5$
 - $F_{\text{West}} = 51 \pm 1$
 - ◆ Include:
 - » Anti-alias filter on photodiode signal
 - » Pendulum response
 - Actuator calibration !
 - ◆ Ignore: locking filters (high freq.)



Sensitivity

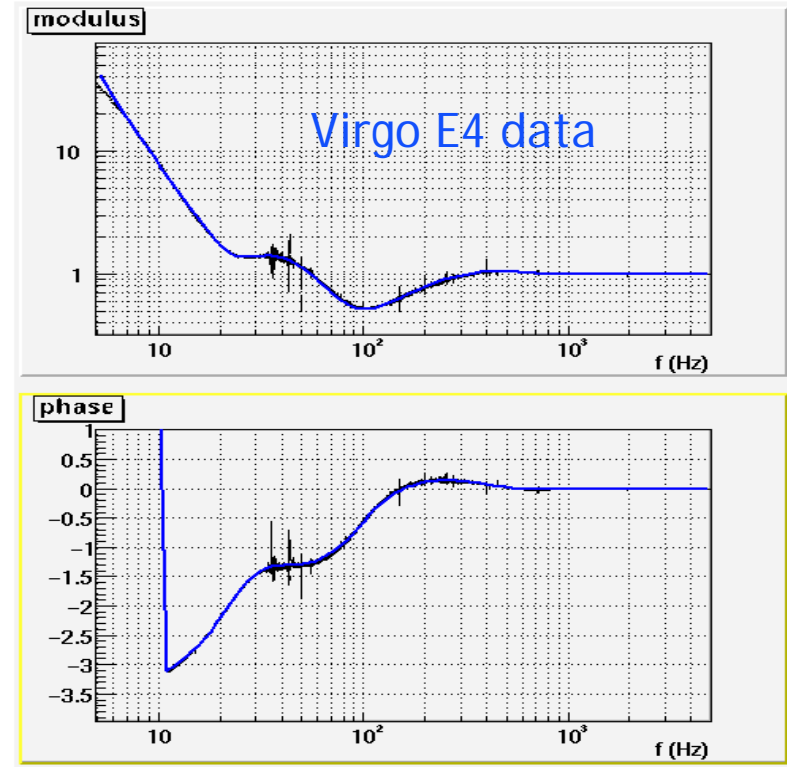
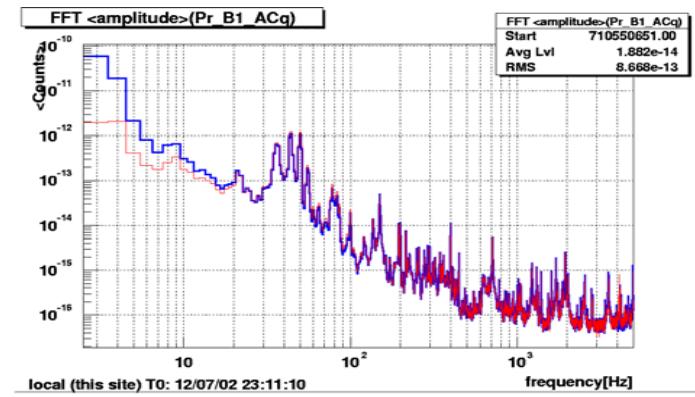
- Apply measured & fitted TF to B1_ACp spectrum
- Remark: Calibrations done injecting noise on NE or WE give different sensitivities
 - ◆ At ~40% level
 - ◆ Assume 14 $\mu\text{m}/\text{V}$ for actuators
 - » WE is probably 15% smaller
 - » Does not explain all of the difference
 - » Work in progress



Building $h(t)$

$h(t)$ reconstruction with filter

- Method:
 - ◆ Fit ITF response with pole-zero model
 - > optical response + locking loop
 - ◆ Convert to Time Domain filters
 - ◆ Apply to dark fringe

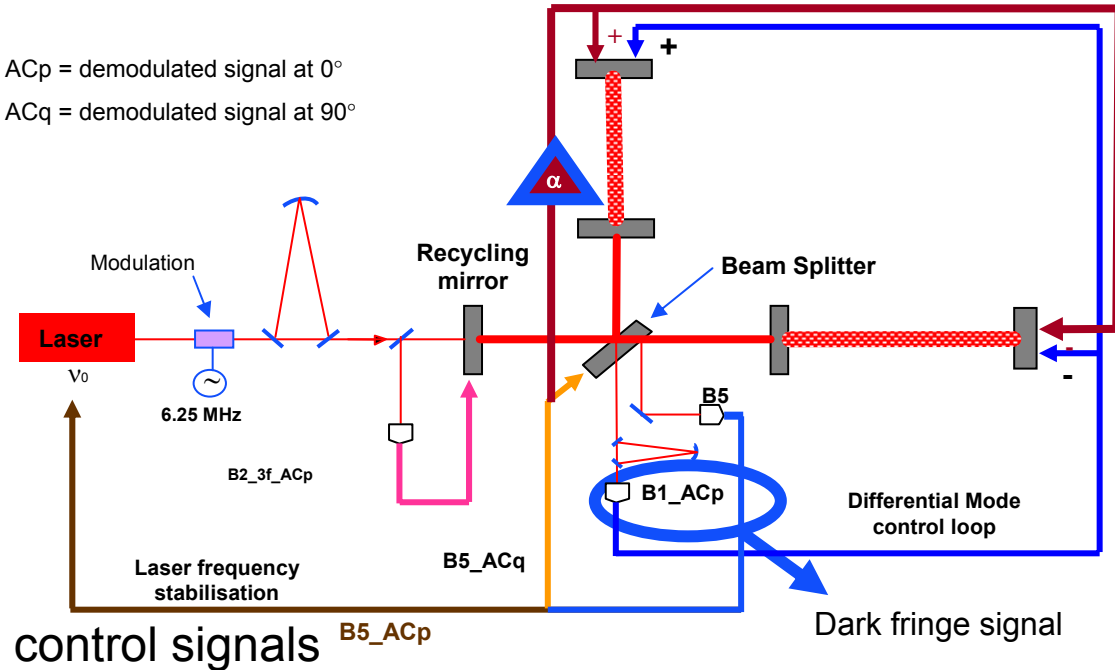


- Problems:
 - ◆ Complicated locking model (coupled loops)
 - ◆ Need to follow the coupling coefficient (the TF shape change with time)
 - ◆ End up with unstable filters

$h(t)$ reconstruction using controls signals

- A locked ITF:

ACp = demodulated signal at 0°
ACq = demodulated signal at 90°



- Dark fringe signal:

 - ◆ Free ITF + effect of the control signals

- Control signals are known

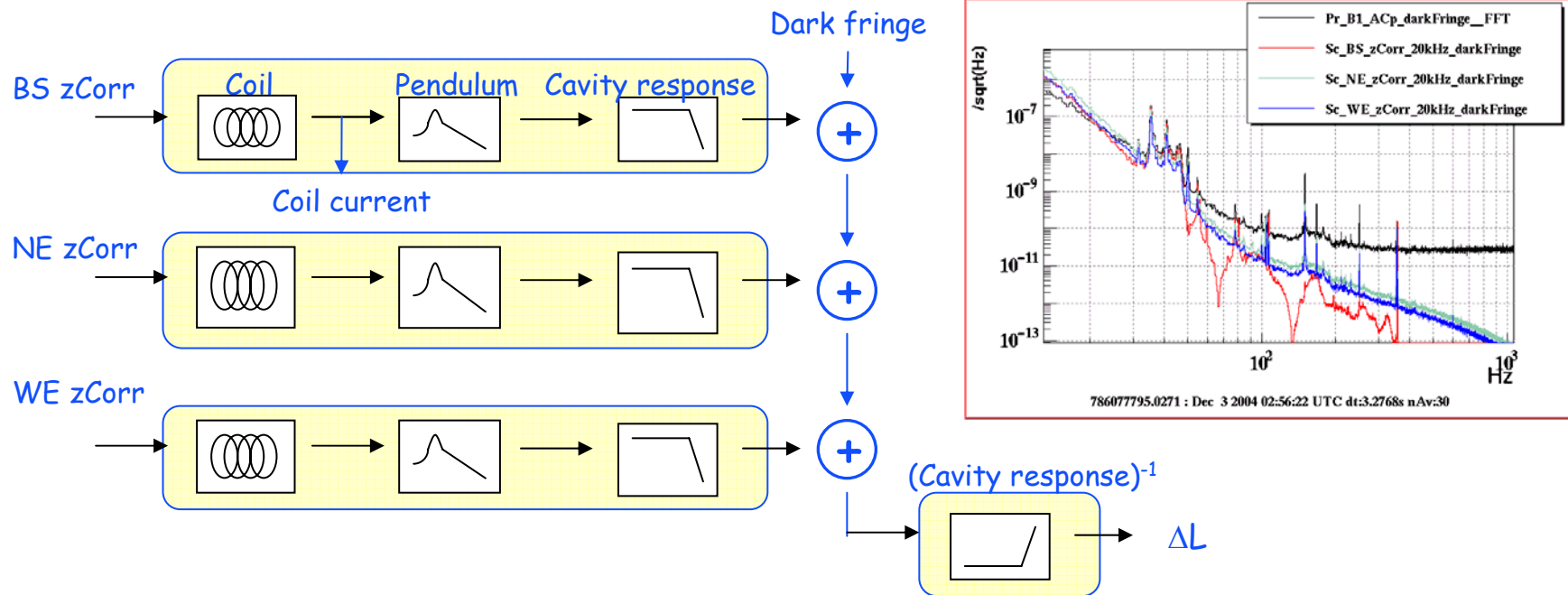
 - ◆ Their effect on the mirrors motion is simple

- Free ITF = Locked ITF – control signal

 - ◆ + correction for the optical response (cavity filtering)

- Remark: this method remove some of the control noises

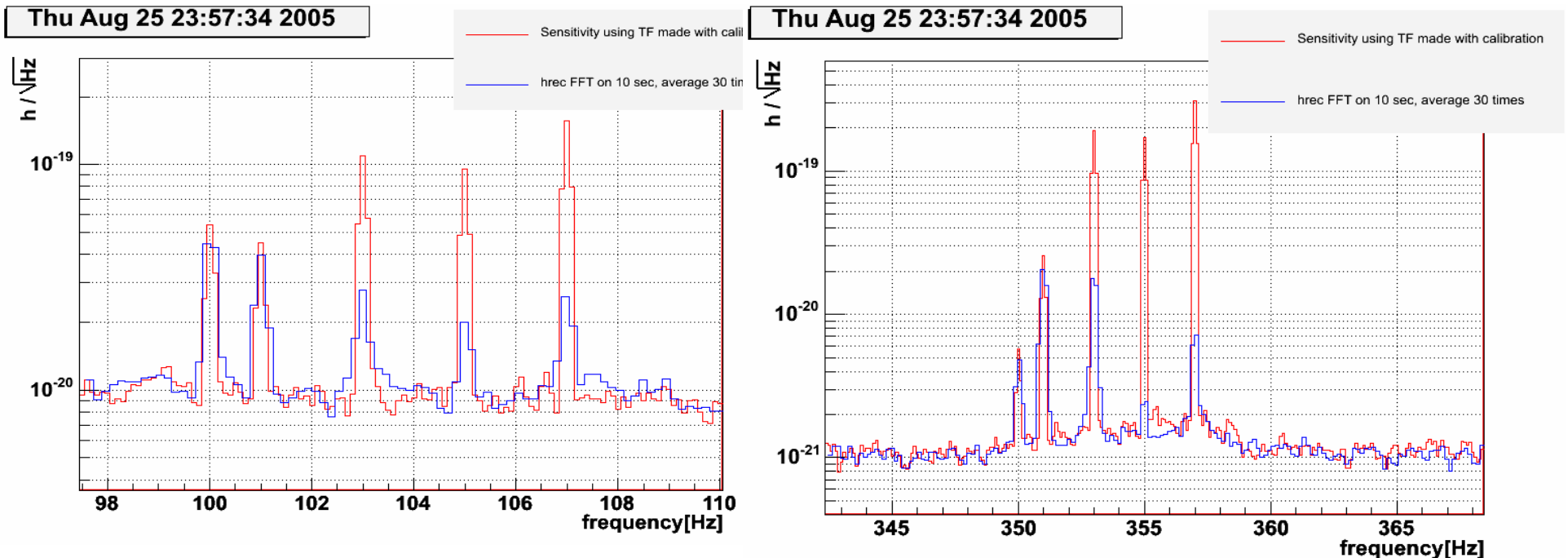
h(t) reconstruction details



- Remove locking effects from dark fringe signal
 - ◆ using mirror correction signal as locking effects measurements
 - ◆ need actuators TF (assuming $14\mu\text{V}$) and optical TF for three mirrors
 - ◆ Track the optical gain with calibration lines
- Convert dark fringe to ΔL
 - ◆ need inverse optical TF (assume a 500 Hz cavity freq. cutoff)

Optical gains tracking

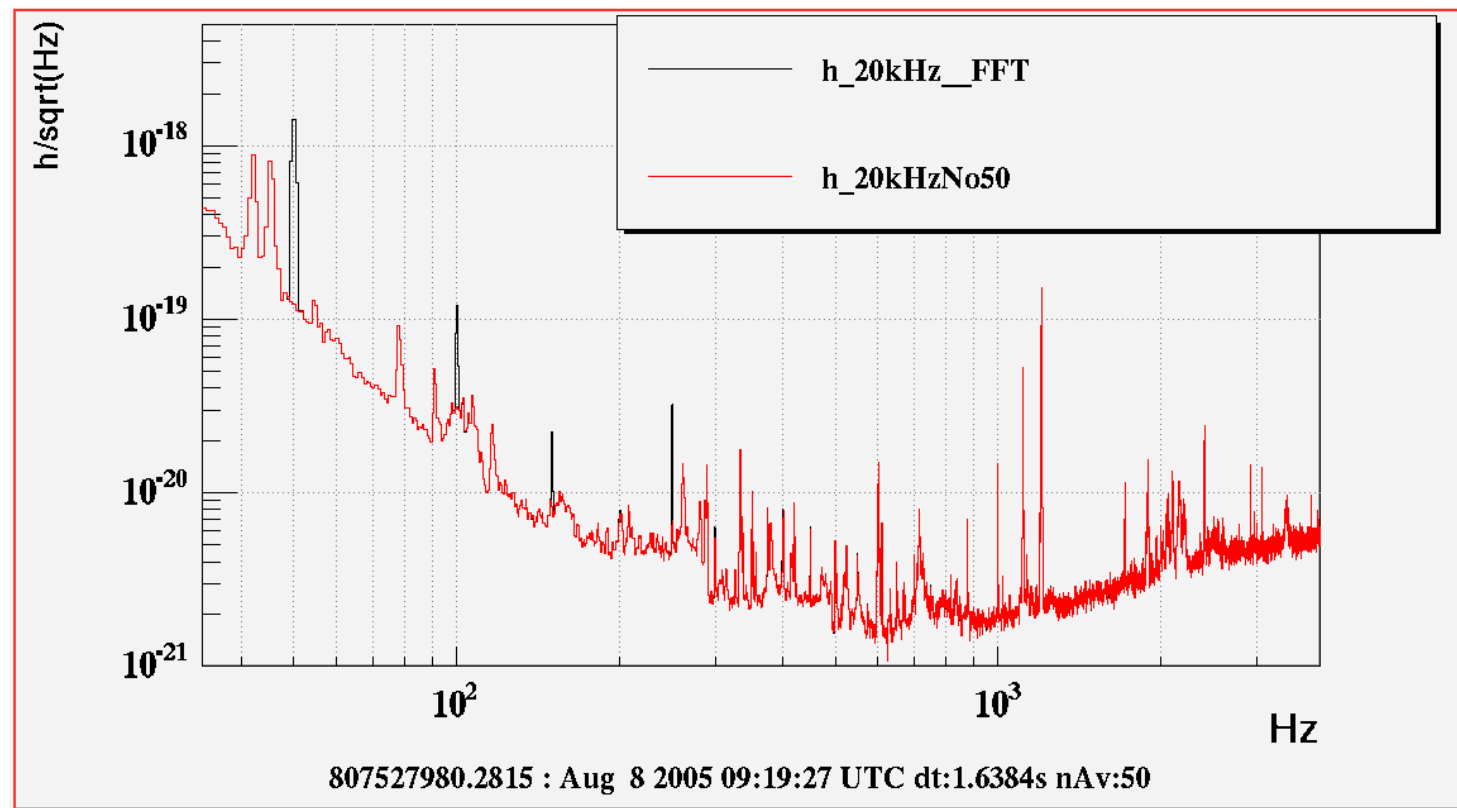
- Monitor calibration lines amplitude in dark fringe and correction signals
 - ⇒ Update the optical gains for BS, NE, WE using the 350 Hz lines
 - ⇒ The “100 Hz” lines are used as a monitor of the quality



- Remark: Calibration lines removed by reconstruction
 - ⇒ Remaining lines amplitude used as error estimators: ~10-15% in WSR1

Additional noise removal: 50Hz lines

- Power line frequency is monitor using an auxiliary channel
- Track the coupling coefficient and phase
- Subtract the power lines in the time domain

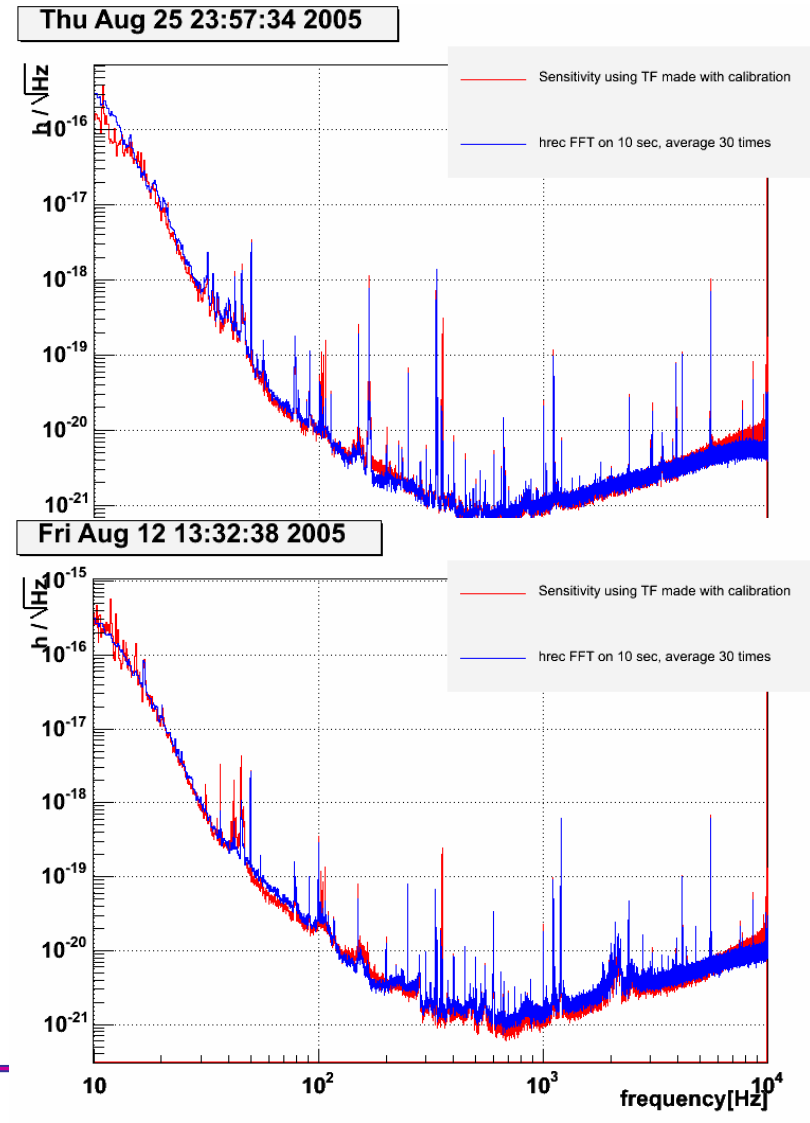


h(t) validation

- 1) Sensitivity vs reconstruction
- 2) Shot noise level
- 3) The photon calibrator
- 4) The hardware injection

Validation 1: Reconstruction vs Sensitivity

- Sensitivity from freq. domain calibration vs $h(t)$ spectrum
- Limits of this comparison:
 - ◆ Sensitivities cannot be compared at exactly the same time
 - » Permanent lines needed for $h(t)$ reconstruction are off when reference spectrum is measured
 - » Interferometer is non-stationary!
 - ◆ Sensitivities depend on different actuator gains
 - » Freq. domain: NE or WE depending on injection point
 - » $h(t)$: average of NE and WE

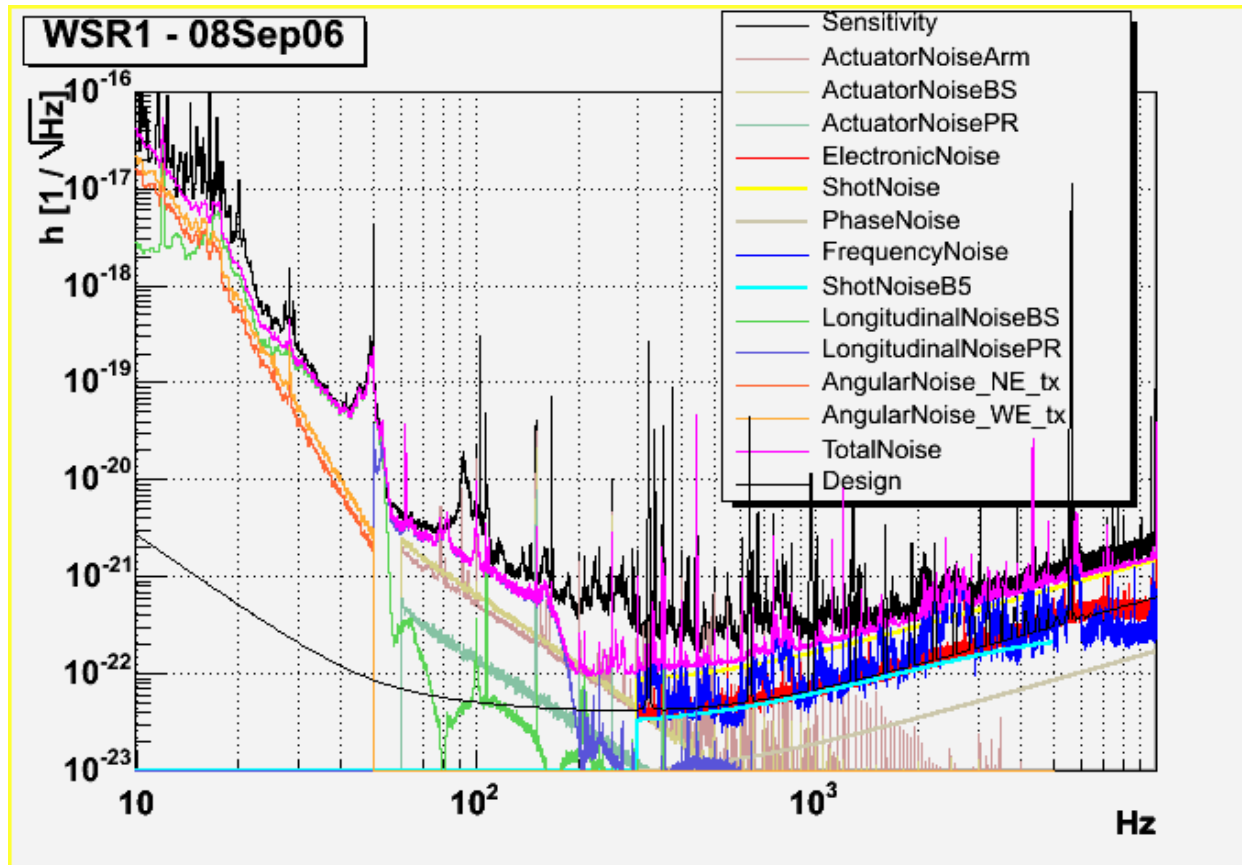


Validation 2: shot noise level

- Noise budget driven by shot noise at high frequency

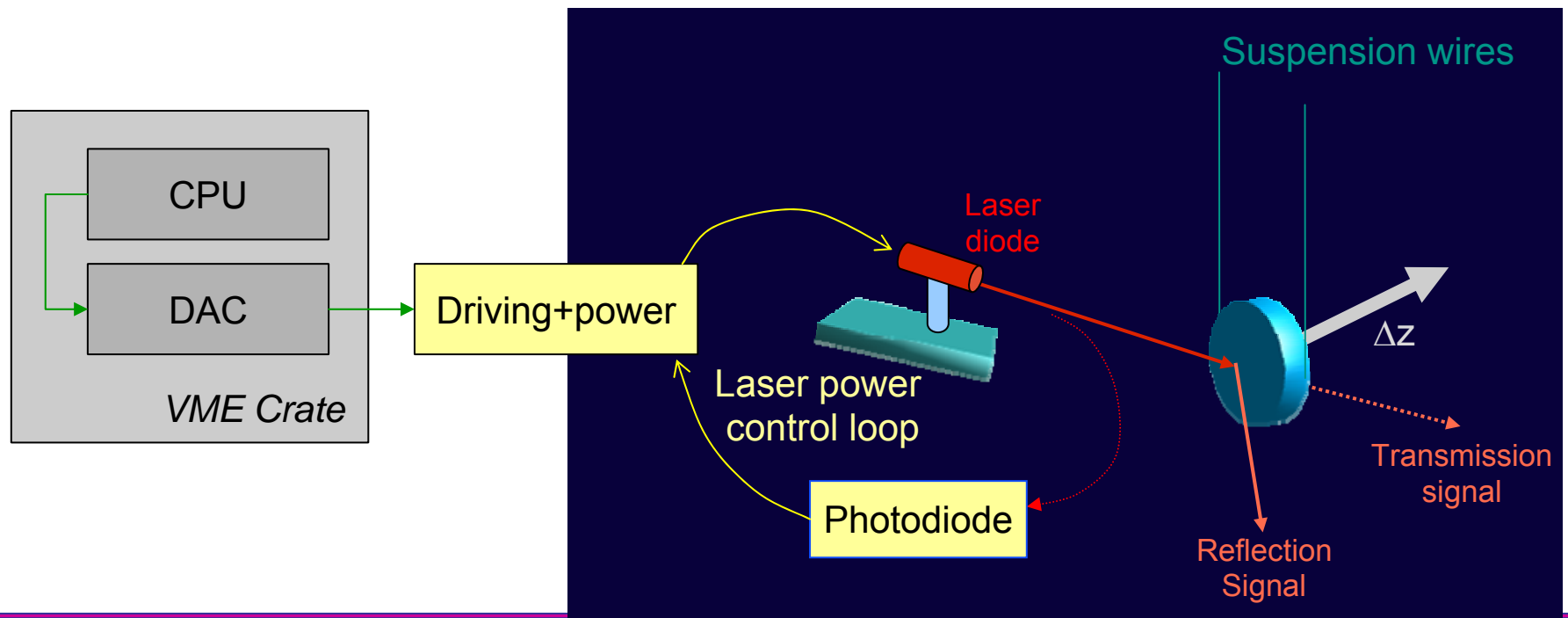
- Shot noise compute with
 - ◆ Output photodiode power
 - ◆ No actuator gain involved
 - ◆ No optical gain involved

- Absolute cross check



Validation 3: The photon calibrator

- Principle: Push the mirror with the radiation pressure of an auxiliary laser beam
- Power modulation



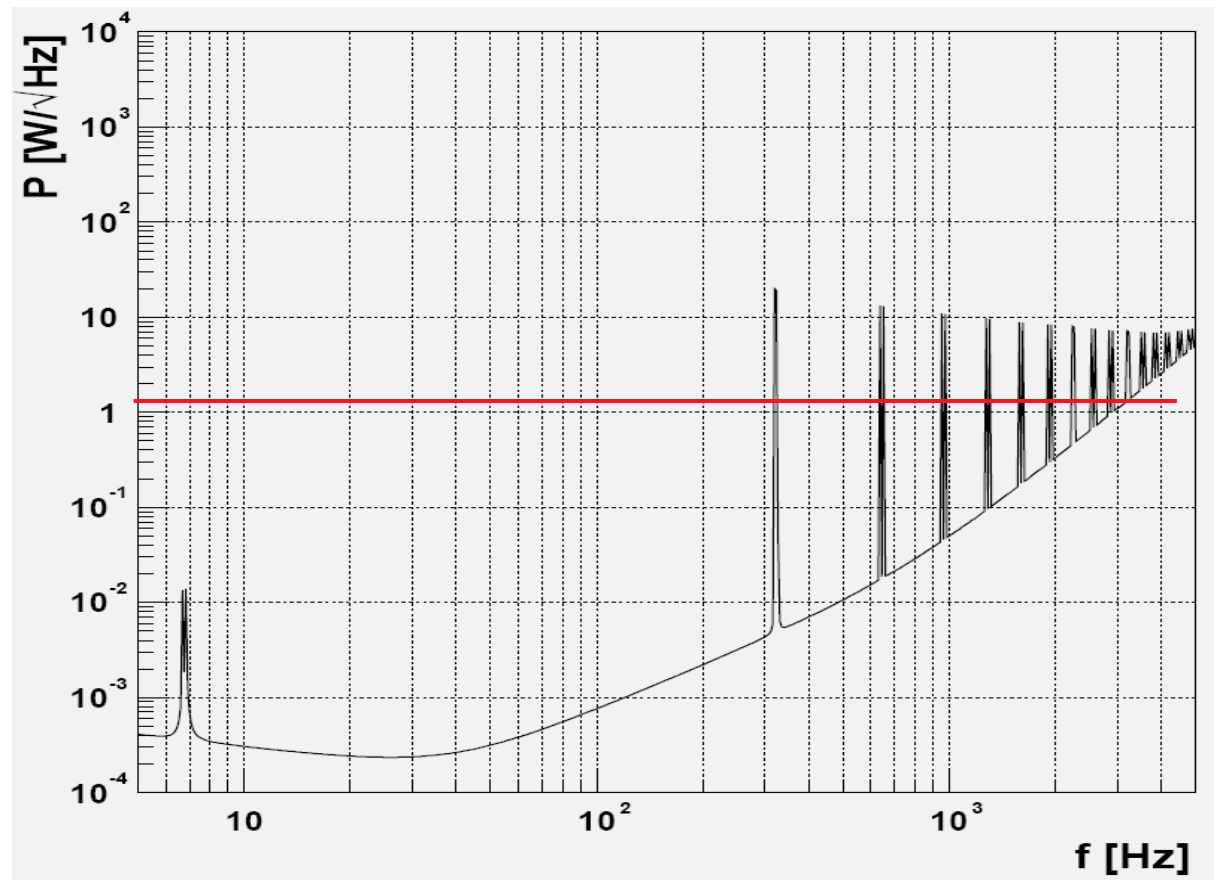
Laser power and design sensitivity

- Needed power to reach Virgo sensitivity:

- ◆ 1 s integration time

- Nominal values

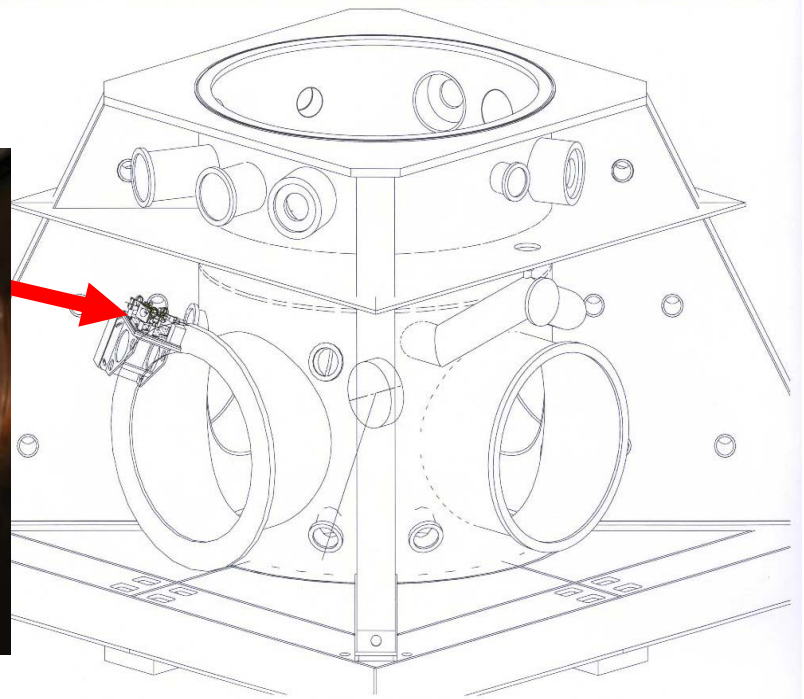
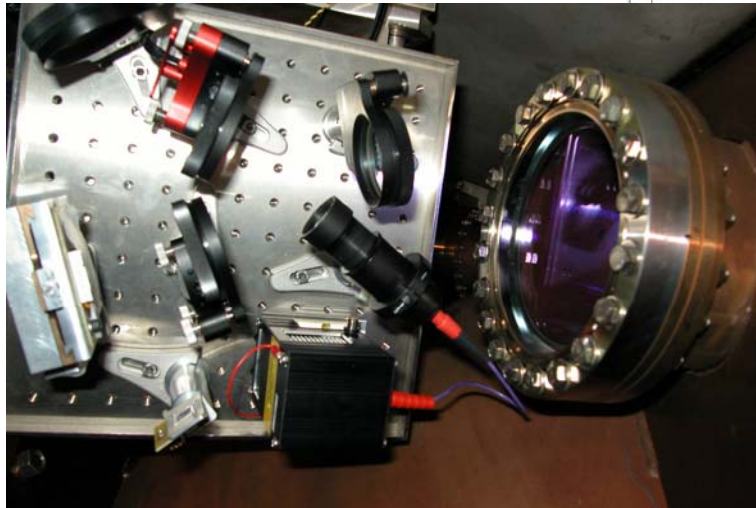
- ◆ $m=20.5$ kg
- ◆ $R\sim 90\%$
- ◆ $P=1.2$ W
- ◆ $i=40^\circ$



Photon calibrators

- In Virgo:

- ◆ Installed but not yet used

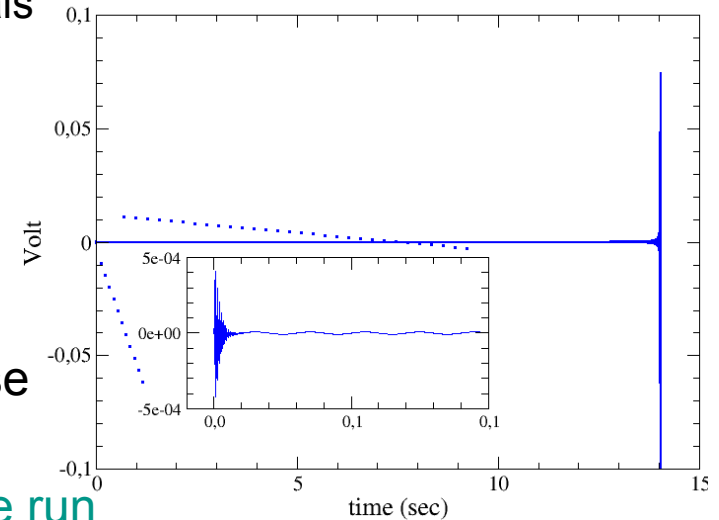


- In LIGO and GEO

- ◆ in general agreement with the classical calibration
- ◆ Work in progress to improve its systematic errors

Validation #4: Hardware injections

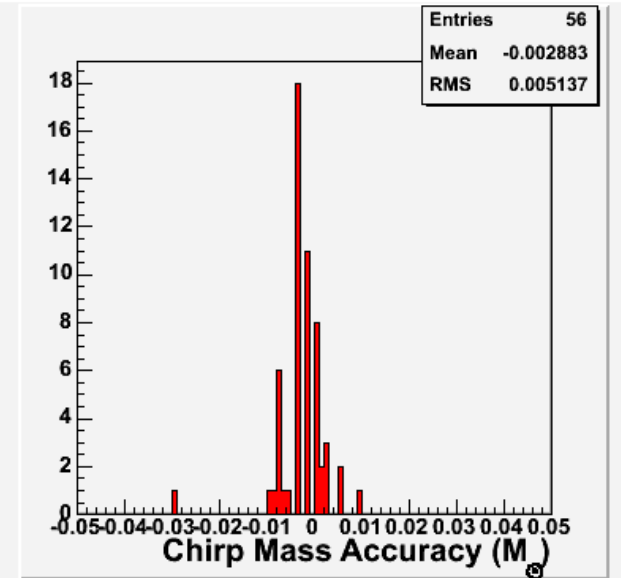
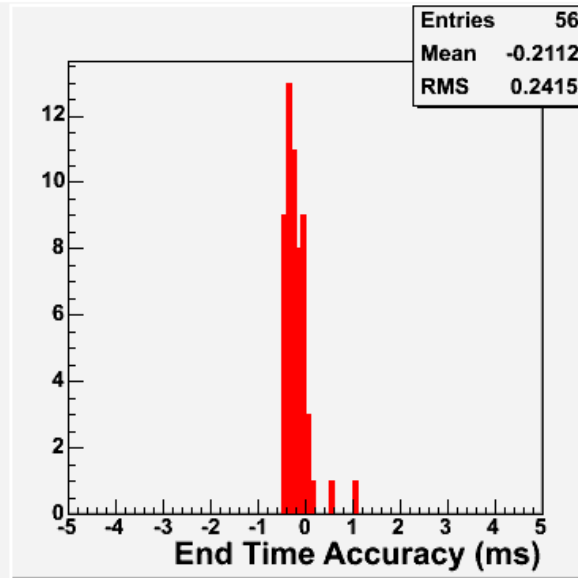
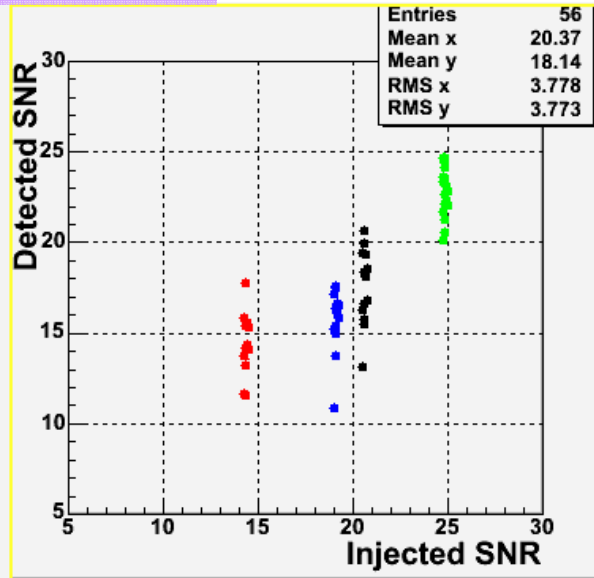
- Idea:
 - ◆ Inject in the ITF known waveform
 - ◆ Done by moving one of the uncontrolled mirror
 - » the $h(t)$ reconstruction removed the control signals
 - ◆ Check the recovered event
- Waveforms:
 - ◆ Use different waveform
 - » Inspiral events sweep the frequency band!
 - ◆ Sending pre-shaped voltages to mirror coils
 - ◆ Takes into account electro-mechanical response
 - ◆ Need to provide a smooth termination
- Normalized with the sensitivity measured before the run
 - ◆ Some changes could be expected
 - ◆ But distance should be recovered
- Check reconstruction and the “pipelines”



Exemple: C6 hardware injections

- 56 inspiral hardware injections
 - ◆ 4 different periods, $[1.4, 1.4] M_{\odot}$, SNR ranging from ~ 15 to 25
 - All detected
 - ◆ Check timing and mass estimation accuracy
 - ◆ Check SNR recovery
- $\sim 10\%$ loss might be due to sensitivity non-stationarity

MBTA



Summary

- $h(t)$ is needed and produced routinely in Virgo
 - ◆ Code running online
 - » Use to produce the online horizon
 - ◆ Data are usually reprocess later on
- $h(t)$ reconstruction provides some noise subtraction
- $h(t)$ is the starting point for the Virgo data analysis
 - ◆ No other calibration parameters are provided
- Tools exist to validate the results
 - ◆ Work is in progress to use all of them